

# Structures within the Quantization Noise: Micro-Chaos in Digitally Controlled Systems <sup>\*</sup>

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**Abstract:** Quantization, sampling and delay in digitally controlled systems can cause undesired oscillations (Csernák and Stépán, 2011), which – depending on the nature of the uncontrolled system – may cause issues of various importance. In many cases, these oscillations can be treated as *quantization noise* (Widrow and Kollár, 2008), and can be handled elegantly with the corresponding quantization theory.

However, we are interested in the structure and patterns of quantization in case of a digitally controlled inverted pendulum with input and output quantizers and sampling. We show the patterns of control effort in case of a simple PD control and highlight how these patterns – along with the dynamics of the controlled system – lead to attractors or periodic cycles with superimposed chaotic oscillations.

*Keywords:* micro-chaos, digital control, sampling, quantization, quantization noise

## 1. INTRODUCTION

Taking delay, quantization and sampling into account in digitally controlled systems is often a challenging step in the accurate mathematical modelling of such systems. In many cases, utilizing faster processors or higher resolution analog-to-digital (ADC) and digital-to-analog (DAC) converters means that the effect of delay, sampling and quantization can be reduced. In these cases, the application of *quantization theory* yields a sophisticated way to analyse these effects (Widrow and Kollár, 2008).

However, we are interested in the underlying patterns of control effort and how to utilize them with the knowledge of the dynamics of the controlled system. We show the general effect of quantization at the input, at the output, and how these sum up on case of input and output quantization. We point out, that even if the region of oscillations caused by quantization is very small, the underlying structure of periodic cycles, chaotic attractors and repellers might yield invaluable information about the qualitative behaviour around the equilibrium.

## 2. DIGITALLY CONTROLLED INVERTED PENDULUM

Consider a 1 DoF inverted pendulum with digital control, sampling and quantization at the measured states and output control effort. The processing delay is neglected and the control realizes *zero-order-hold*, see Fig. 1. Therefore,

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the system can be illustrated with the block diagram in Fig. 2. The measured angle  $\varphi$  and angular velocity  $\dot{\varphi}$  are quantized with input resolution  $r_I$ , and the calculated control effort  $M$  is also quantized with output resolution  $r_O$ .

After linearization, the equation of motion of the inverted pendulum is:

$$\ddot{\varphi}(t) + 2\delta\alpha\dot{\varphi}(t) - \alpha^2\varphi(t) = -(P\varphi_i + D\dot{\varphi}_i) \quad t \in [i\tau, (i+1)\tau), \quad (1)$$

where  $\alpha$  is the natural frequency,  $\delta$  is the relative damping,  $P$  and  $D$  are control parameters,  $\tau$  is the sampling time and Eq. (1) is valid between subsequent sampling instants. Introducing the dimensionless time  $T = t/\tau$ , and using the notation:  $\square' = d\square/dT$ , Eq. (1) can be written as:

$$\varphi''(T) + 2\delta\hat{\alpha}\varphi'(T) - \hat{\alpha}^2\varphi(T) = -(\hat{P}\varphi_i + \hat{D}\dot{\varphi}'_i) \quad T \in [i, i+1), \quad (2)$$

where  $\hat{\alpha} = \alpha\tau$ ,  $\hat{P} = P\tau^2$ ,  $\hat{D} = D\tau$ . Adding the input and output quantization to Eq. (2) yields:

$$\varphi''(T) + 2\delta\hat{\alpha}\varphi'(T) - \hat{\alpha}^2\varphi(T) = -r_O\tau^2 \text{Int} \left( \frac{Pr_I}{r_O} \text{Int} \left( \frac{\varphi_i}{r_I} \right) + \frac{Dr_I}{\tau r_O} \text{Int} \left( \frac{\dot{\varphi}'_i}{r_I} \right) \right).$$

Here the resolution of quantization at the input is  $r_I$  and at the output  $r_O$ . In order to reduce the number of parameters, re-scale the space coordinate:  $x = \varphi/X$ , ( $x' = \varphi'/X$ ,  $x'' = \varphi''/X$ ).

$$x''(T) + 2\delta\hat{\alpha}x'(T) - \hat{\alpha}^2x(T) = -\frac{r_O\tau^2}{X} \text{Int} \left( \frac{Pr_I}{r_O} \text{Int} \left( \frac{x_i X}{r_I} \right) + \frac{Dr_I}{\tau r_O} \text{Int} \left( \frac{x'_i X}{r_I} \right) \right)$$

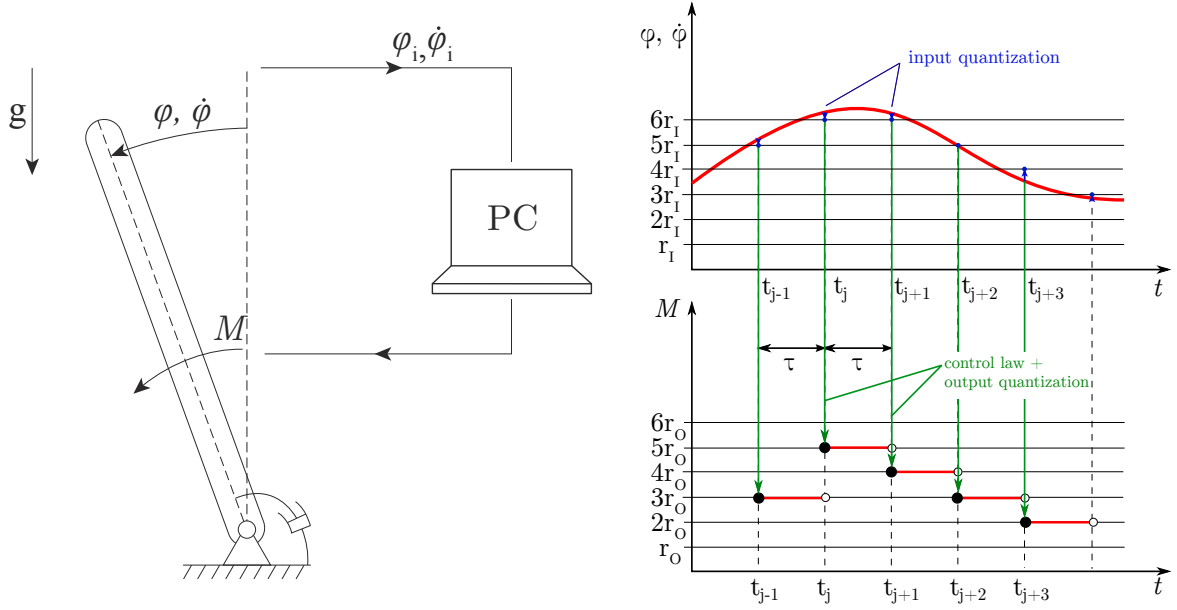


Fig. 1. The digitally controlled inverted pendulum with zero-order-hold.

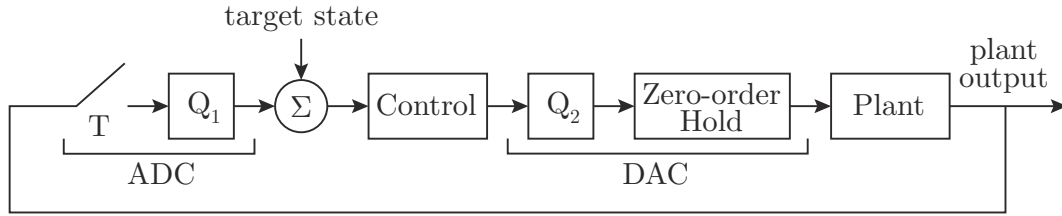


Fig. 2. Control flow including analog-to-digital conversion of  $\varphi$  and  $\dot{\varphi}$ , and digital-to-analog conversion of the calculated control effort  $M$ .

In order to make the output quantization dimensionless, let  $X = r_O \tau^2$ :

$$x''(T) + 2\delta\hat{\alpha}x'(T) - \hat{\alpha}^2x(T) = -\text{Int}\left(\frac{P r_I}{r_O} \text{Int}\left(\frac{x_i r_O \tau^2}{r_I}\right) + \frac{D r_I}{\tau r_O} \text{Int}\left(\frac{x'_i r_O \tau^2}{r_I}\right)\right).$$

Introducing  $\rho_I = r_I/(r_O \tau^2) = r_I/X$  one can write:

$$x''(T) + 2\delta\hat{\alpha}x'(T) - \hat{\alpha}^2x(T) = -\text{Int}\left(P \tau^2 \rho_I \text{Int}\left(\frac{x_i}{\rho_I}\right) + D \tau \rho_I \text{Int}\left(\frac{x'_i}{\rho_I}\right)\right).$$

Here  $\hat{P}$  and  $\hat{D}$  can be recognized and it can be seen, that  $\rho_I$  acts as a resolution for the input quantization:

$$x''(T) + 2\delta\hat{\alpha}x'(T) - \hat{\alpha}^2x(T) = -\text{Int}\left(\hat{P} \rho_I \text{Int}(x_i/\rho_I) + \hat{D} \rho_I \text{Int}(x'_i/\rho_I)\right). \quad (3)$$

### 3. MICRO-CHAOS MAP

Equation (3). represents the inverted pendulum with sampling, PD-control and quantization at both input and output. Rewriting it as a system of first order differential equations one can formulate its solution as:

$$\mathbf{y}(T) = \mathbf{U}(T)\mathbf{y}(0) + \mathbf{b}(T)F(T), \quad T \in [0, 1), \quad (4)$$

where  $\mathbf{y} = [x(T) \quad x'(T)]^T$ ,  $\Gamma = \sqrt{1 + \delta^2}$  and:

$$\mathbf{U}(T) = \frac{e^{-\hat{\alpha}\delta T}}{\Gamma} \begin{bmatrix} \Gamma \text{ch}(\hat{\alpha}\Gamma T) + \delta \text{sh}(\hat{\alpha}\Gamma T) & \text{sh}(\hat{\alpha}\Gamma T)/\hat{\alpha} \\ \hat{\alpha} \text{sh}(\hat{\alpha}\Gamma T) & \Gamma \text{ch}(\hat{\alpha}\Gamma T) - \delta \text{sh}(\hat{\alpha}\Gamma T) \end{bmatrix},$$

$$\mathbf{b}(T) = \frac{1}{\hat{\alpha}^2 \Gamma} \begin{bmatrix} \Gamma - e^{-\hat{\alpha}\delta T} (\Gamma \text{ch}(\hat{\alpha}\Gamma T) + \delta \text{sh}(\hat{\alpha}\Gamma T)) \\ -\hat{\alpha} e^{-\hat{\alpha}\delta T} \text{sh}(\hat{\alpha}\Gamma T) \end{bmatrix}.$$

Substituting  $T = 1$ , the so-called *micro-chaos map* (Haller and Stépán, 1996) is obtained, which is valid at sampling instants:

$$\mathbf{y}_{i+1} = \mathbf{U}(1)\mathbf{y}_i + \mathbf{b}(1)F_i, \quad (5)$$

$$F_i = \text{Int}\left(\rho_I (\hat{P} \text{Int}(x_i/\rho_I) + \hat{D} \text{Int}(x'_i/\rho_I))\right),$$

where  $F_i$  is the control effort at sampling time  $i$ .

### 4. PATTERNS OF CONTROL EFFORT DUE TO QUANTIZATION

Before examining the behaviour of the *micro-chaos map* Eq. (5), let us visualise the quantized control effort and show the switching lines between bands of the same values.

In this paper, we use a mid-tread quantizer with double dead zone, that is  $\text{Int}(x)$  yields the integer part of  $x$  (see Fig. 3).

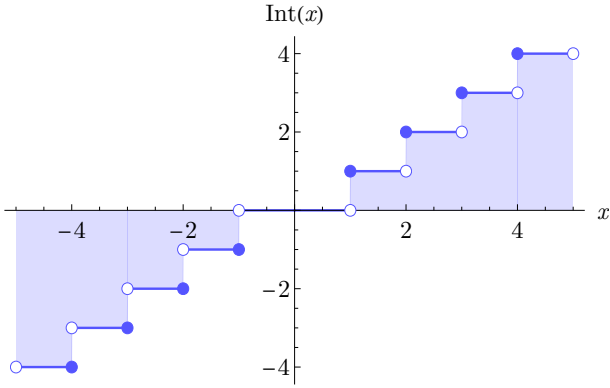


Fig. 3. Mid-tread quantizer with double dead zone – IntegerPart function.

It is clear that for low  $\rho_I$  values, the output quantization *dominates* and therefore the switching lines can be given as:

$$F = \hat{P}x + \hat{D}x' \quad F \in \mathcal{Z} \setminus \{0\}, \quad (6)$$

the slope of the switching lines are determined by the control parameters. In case of  $\hat{D} = 0$ , the switching lines are vertical, and in case of  $\hat{P} = 0$  the switching lines are horizontal in the  $(x, x')$  state space. The regions corresponding to the same control effort are stripes or bands between the switching lines.

On the other hand, for high  $\rho_I$  values, the *input quantization* dominates and the switching lines are forming a grid at  $x = i\rho_I$  and  $x' = j\rho_I$ . That is, regions in the state space corresponding to the same control effort are squares (or rectangles due to the double dead zone).

If we look at the transition between the above mentioned cases, with increasing the value of  $\rho_I$ , a special kind of bifurcation (*"border-border-collision"*) can be observed. As the switching lines become more and more *jagged*, eventually they will touch each other, and a contiguous control band falls apart into rectangular regions. We have found the first critical value to be:

$$\rho_I^* = 1/\hat{P}, \quad (7)$$

and it can be also shown, that  $\rho_{I,k}^* = k/\hat{P}$ , ( $k \in \mathcal{Z}$ ) yields similar regular patterns, where  $k^{\text{th}}$  the corners of the *jagged* switching lines touch each other.

This kind of bifurcation enables the dynamics to *step over* certain control values when passing the switching lines at the proper locations, see Fig. 6. By increasing  $\rho_I$  beyond the critical  $\rho_I^*$  value, the disappearance of certain control value regions can be observed, see Fig. 5, where only control value regions  $F \bmod 5 = 0$  can be seen.

Based on former research (Haller and Stépán, 1996; Csernák and Stépán, 2010, 2012; Gyebrošzki and Csernák, 2014) it is known, that in the case of output quantization, multiple chaotic attractors can be found in the state space, at the intersections of switching lines and the  $x$  axis, see Fig. 7.

Depending on system and control parameters, attractors may appear or disappear due to border-collision bifurcation (De Almeida, 1990), or some of them may become repellers, and form one or more bigger attractors, by

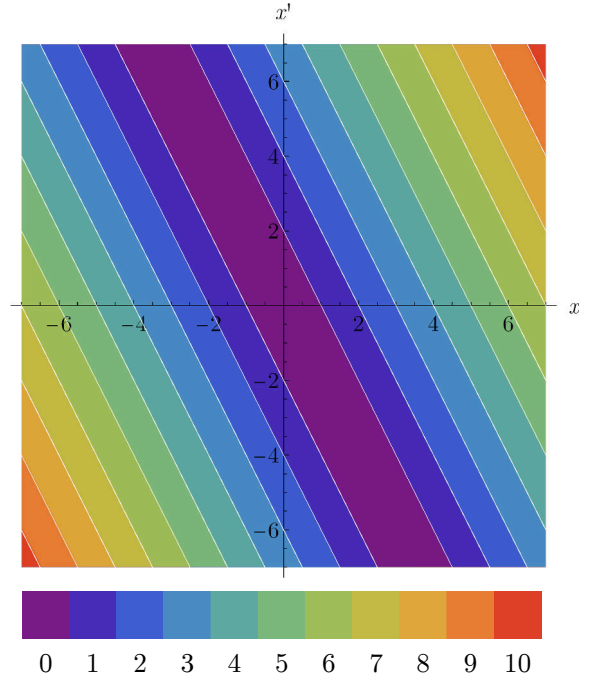


Fig. 4. Switching lines in case of dominating input quantization:  $\hat{P} = 1$ ,  $\hat{D} = 0.5$ ,  $r_I = 0.0001$ ,  $r_O = 1$ . The bands of the same control effort are stripes. Color scale shows the magnitude of the control effort:  $|F|$ .

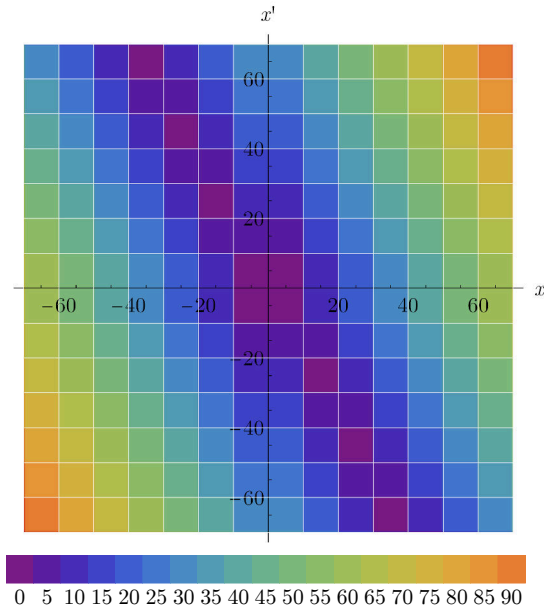


Fig. 5. Switching lines in case of dominating output quantization:  $\hat{P} = 1$ ,  $\hat{D} = 0.5$ ,  $r_I = 10$ ,  $r_O = 1$ . The regions of the same control effort are squares, (or rectangles around the axes due to the double dead zone). Color scale shows the magnitude of the control effort:  $|F|$ .

pushing the trajectory towards each other (Csernák et al., 2016).

In case of input quantization, our general observation is that a periodic orbit (with superimposed chaotic oscillations) appears around the internal structure of repellers.

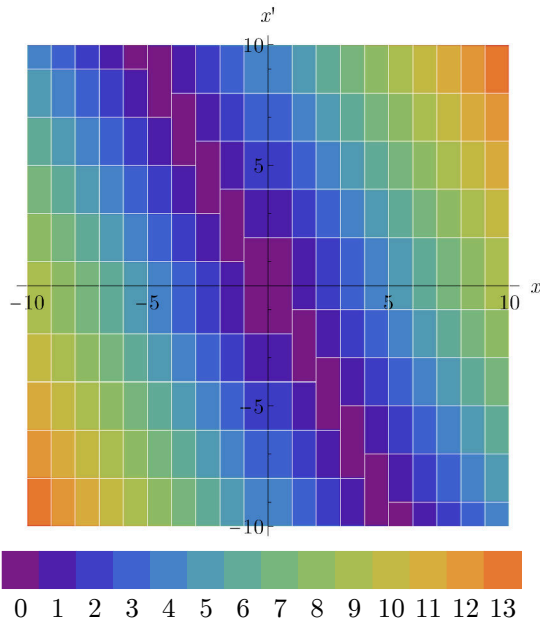


Fig. 6. Switching lines in case of critical  $\rho_1^* = 1/\hat{P}$ ,  $\hat{P} = 1$ ,  $\hat{D} = 0.5$ . The control effort bands fall apart into a set of rectangles. Color scale shows the magnitude of the control effort:  $|F|$ .

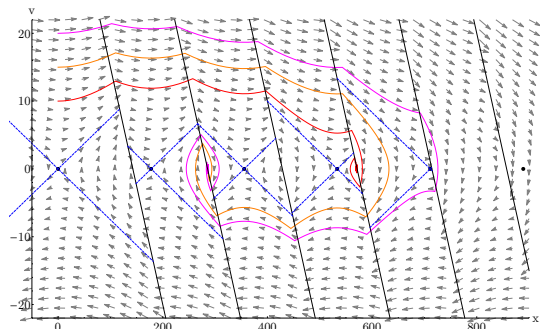


Fig. 7. State space of the micro-chaos map:  $\hat{\alpha} = 0.075$ ,  $\delta = 0.03$ ,  $\hat{P} = 0.007$ ,  $\hat{D} = 0.02$ ,  $r_I \rightarrow 0$ ,  $r_O = 1$ . Three example trajectories are shown starting from  $x = 0$  and  $\blacksquare$ :  $x' = 10$ ,  $\blacksquare$ :  $x' = 15$ ,  $\blacksquare$ :  $x' = 20$ . Two of them ( $\blacksquare$ ) end up in an attractor on the switching line between bands of control effort  $F = 1, 2$ , while the one starting closest to the origin ( $\blacksquare$ ) ends up in an attractor between bands  $F = 3, 4$ .

Depending on the parameters, a single chaotic attractor spanning over multiple control effort bands can be found, see Fig. 10.

By carrying out numerical simulations it can be seen, how rich the dynamics behind the *micro-chaos map* is, as one varies the parameter  $\rho_1$  which corresponds to the ratio of resolutions of the input and output quantization.

Although the analysis of a certain state space region – finding all fixed points, periodic orbits, attractors or repellers – is inefficient by running numerical simulations, hence we have utilized Cell Mapping methods (Hsu (1987); Nusse and Yorke (1996); Zou and Xu (2009); de Kraker et al. (2000); Gyebroński and Csernák (2014)) to examine the state space of the micro-chaos map.

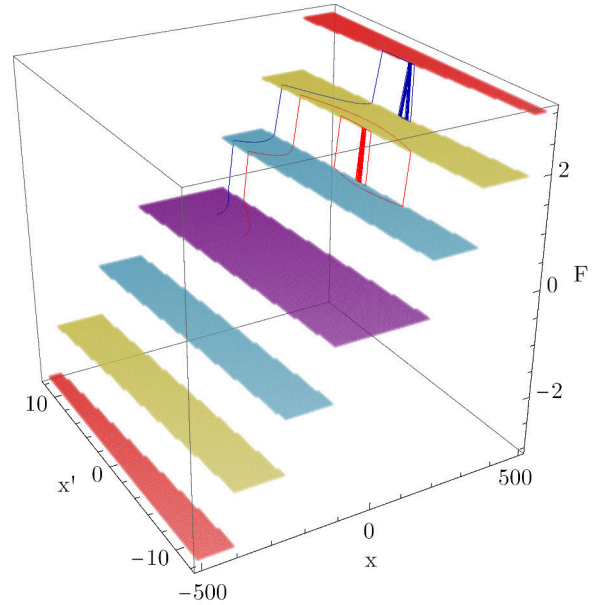


Fig. 8. Example trajectories of the micro-chaos map, leading to two separate attractors in case of  $\hat{\alpha} = 0.07$ ,  $\delta = 0$ ,  $\hat{P} = 0.007$ ,  $\hat{D} = 0.02$ ,  $\rho_1 = 0.001$ . Initial states:  $x = 0$  and  $\blacksquare$ :  $x' = 4$ ,  $\blacksquare$ :  $x' = 8$ . Coloured layers show bands of same control effort values  $F$ .

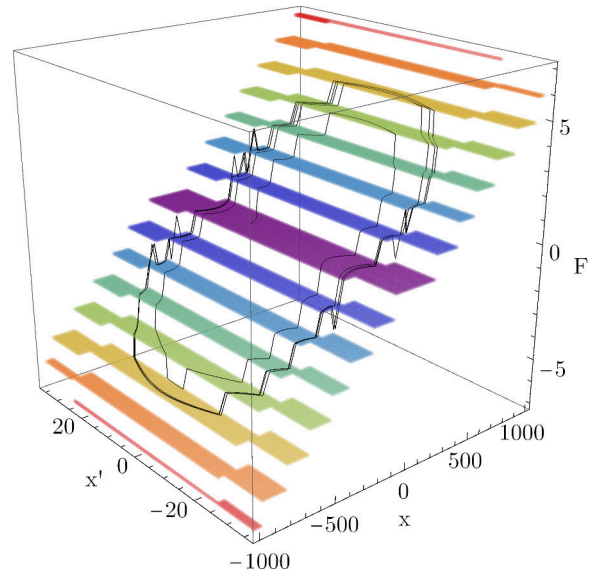


Fig. 9. Example trajectory of the micro-chaos map, leading to a periodic cycle with chaotic oscillation superimposed.  $\hat{\alpha} = 0.07$ ,  $\delta = 0$ ,  $\hat{P} = 0.007$ ,  $\hat{D} = 0.04$ ,  $\rho_1 = 25$ . Initial state  $x = 0$  and  $x' = 10$ . Coloured layers show bands of same control effort values  $F$ .

## 5. CELL MAPPING RESULTS

Cell Mapping (Hsu, 1987) is a technique for the global analysis of dynamical systems. It involves discretization of a selected region of the state space (into *cells*), then one or more *image cells* – where the dynamics lead to – are determined for every cell.

In case of Simple Cell Mapping (SCM), one image cell is determined for every cell, by starting a trajectory from the center of the cell, therefore the intermediate result of SCM

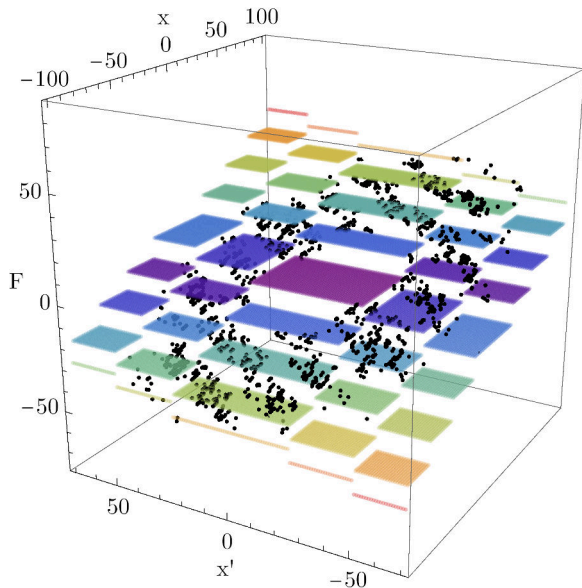


Fig. 10. Example trajectory of the micro-chaos map, leading to a chaotic attractor spanning over multiple control bands.  $\hat{\alpha} = 0.07$ ,  $\delta = 0$ ,  $\hat{P} = 0.4$ ,  $\hat{D} = 0.25$ ,  $\rho_I = 25$ . Initial state  $x = 0$  and  $x' = 150$ . Coloured layers show bands of same control effort values  $F$ .

is a graph. By analysing that graph, one can determine periodic cycles ( $n$ -P groups consisting of  $n$  cells) and transient cells (which lead to a periodic group) forming the basin of attraction of periodic groups. The region outside the examined state space area is called *sink cell*.

Utilizing SCM, we have examined the state space of the *micro-chaos map* for various  $\rho_I$  values and realistic system parameters ( $\hat{\alpha} = 0.07$ ,  $\delta = 0$ ,  $\hat{P} = 0.007$ ,  $\hat{D} = 0.02$ ). As the ratio corresponding to the two resolutions increase, one can observe the transition from separate attractors to an enclosing periodic orbit with chaotic oscillations.

Figure 11. shows a case, when the output quantization is dominant, and there are six chaotic attractors in the state space. As the input quantization gains significance, the switching lines start to become *jagged* – resembling to a *staircase* or a *zigzag* – see Fig. 12. At this point the outermost chaotic attractors disappear due to a structural change in where the stable and unstable manifolds of the nearest saddle point intersect the *jagged* switching line.

Further increasing the value of  $\rho_I$ , the internal structure becomes a set of repellers and an enclosing periodic orbit appears, see Fig. 13. The reason of this is the increased dead zone around the  $x$  axis, which effectively means that the control is only proportional there.

## 6. CONCLUSION

We have presented the *micro-chaos map* corresponding to a digitally controlled inverted pendulum, with input and output quantization, and zero-order hold PD-control. The map itself shows colourful dynamical behaviour which is strongly related to the underlying patterns of control effort caused by the twofold quantization.

An important observation is, that the ratio of the quantizer resolutions has a critical value ( $\rho_I^*$ , Eq. (7)), which corresponds to a special kind of bifurcation, where the corners of *jagged* switching lines are touching each other, allowing the dynamics to bypass certain control effort values.

Cell Mapping methods were used to examine the state space during the variation of  $\rho_I$  and the transition from separate attractors to repellers surrounded by a chaotic attractor was shown. Cell mapping results enable us to qualitatively observe the resulting state space structure and determine the significance of the quantization(s) with respect to the applied control function.

## ACKNOWLEDGEMENTS

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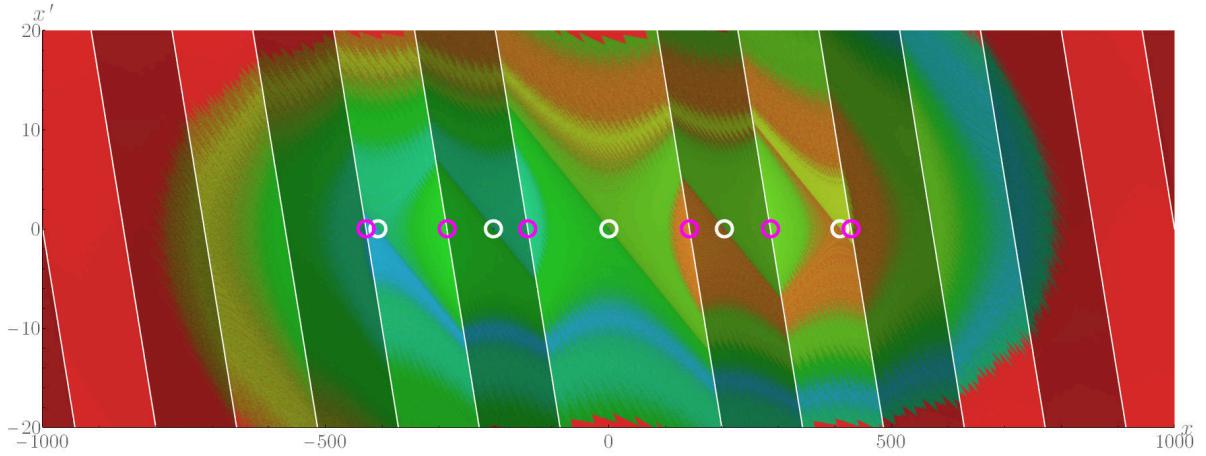


Fig. 11. SCM result in case of  $\hat{\alpha} = 0.07$ ,  $\delta = 0$ ,  $\hat{P} = 0.007$ ,  $\hat{D} = 0.02$ ,  $\rho_I = 0.1$ . There are 6 chaotic attractors highlighted with pink circles, their basin of attraction is coloured from left, to right along the  $x$  axis: ■, ■, ■, ■, ■, ■. The control bands  $F$  are indicated with alternating shades. The fixed points are highlighted with white circles. Red ■ colour indicates transient cells leading to the sink cell.

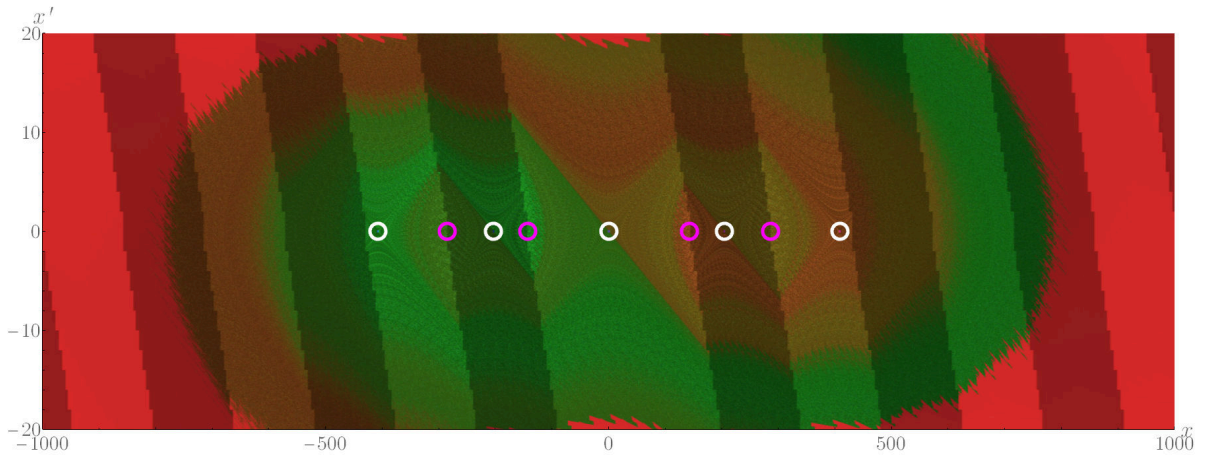


Fig. 12. SCM result in case of  $\hat{\alpha} = 0.07$ ,  $\delta = 0$ ,  $\hat{P} = 0.007$ ,  $\hat{D} = 0.02$ ,  $\rho_I = 2$ . There are 4 chaotic attractors (from left to right: ■, ■, ■, ■), the leftmost and rightmost ones became repellers. The control bands  $F$  are indicated with alternating shades. It can be observed, that the switching lines become *staircase like* or *fragmented*. The control bands  $F$  are indicated with alternating shades. Red ■ colour indicates transient cells leading to the sink cell.

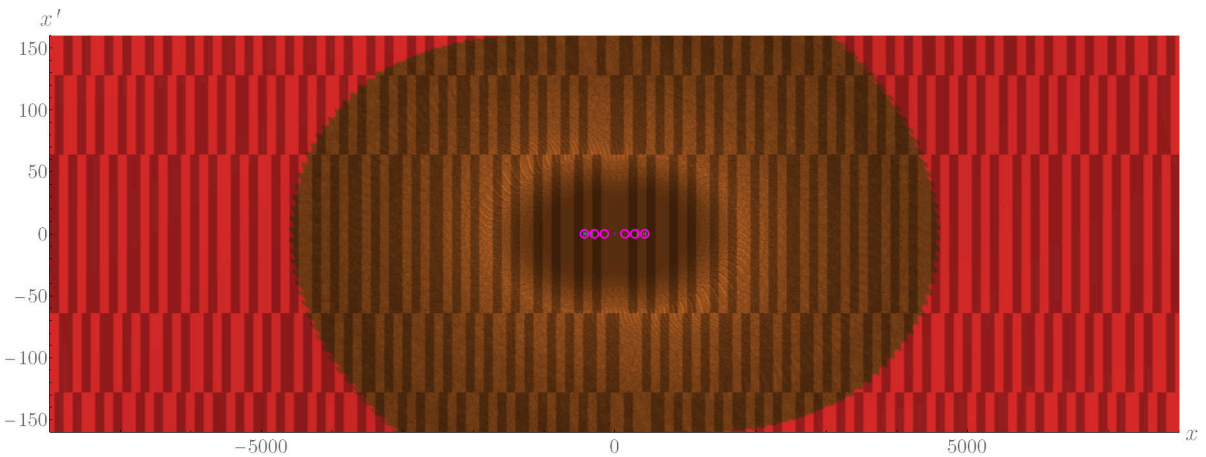


Fig. 13. SCM result in case of  $\hat{\alpha} = 0.07$ ,  $\delta = 0$ ,  $\hat{P} = 0.007$ ,  $\hat{D} = 0.02$ ,  $\rho_I = 64$ . It can be seen, that the method found some internal periodic groups without basin of attraction: these are the remains of the original attractor structure turning to repellers. The state space is attracted by a single periodic cycle coloured with ■ which encloses the internal structure. Red ■ colour indicates transient cells leading to the sink cell.